

# SHEAR AND TORSION IN THICK-WALLED CROSS-SECTIONS (GENERAL FORMULATION)

We consider a thick-walled cross-section of area  $A$  with shear center at  $(y_{sc}, z_{sc})$ . The boundary condition of zero external shear traction is imposed:  $T = 0$  on  $\partial A$ . The axes  $y, z$  are not principal, so the product of inertia  $I_{yz} \neq 0$ . The shear modulus is  $G$ .

## NOTATION

$V_y, V_z$	shear resultants (forces) in $y$ and $z$
$T_w$	warping torsional moment
$T_1$	Saint-Venant (primary) torsion
$I_y, I_z$	second moments of area about $y$ and $z$
$I_{yz}$	product of inertia (nonzero for nonprincipal axes)
$I_w$	warping constant (sectorial moment of inertia)
$\omega(y, z)$	primary warping function (from Section 1)
$u(y, z)$	additional axial displacement (from Section 2)
$u_{total}$	total axial displacement
$\tau_{xy}, \tau_{xz}$	shear stresses

## 1 PRIMARY WARPING $\omega(y, z)$ DUE TO PRIMARY TORSION $T_1$

### 1.1 Weak (variational) formulation

Find  $\omega \in H^1(A)$  such that for all  $\delta w \in H^1(A)$ :

$$\int_A G \nabla \delta w \cdot \nabla \omega \, dA - \int_A G \left[ (y - y_{sc}) \frac{\partial(\delta w)}{\partial z} - (z - z_{sc}) \frac{\partial(\delta w)}{\partial y} \right] dA = 0.$$

The boundary term vanishes because  $T = 0$  on  $\partial A$ .

### 1.2 Strong formulation (Laplace equation)

The warping function  $\omega$  satisfies:

$$\nabla^2 \omega = 0 \quad \text{in } A \quad (\text{Laplace equation})$$

with natural (Neumann) boundary condition:

$$\frac{\partial \omega}{\partial n} = (y - y_{sc}) n_z - (z - z_{sc}) n_y \quad \text{on } \partial A$$

where  $\mathbf{n} = (n_y, n_z)$  is the outward unit normal to  $\partial A$ .

### 1.3 Relation with the Saint-Venant torsion $T_1$

The rate of twist  $\theta' = \frac{d\theta}{dx}$  is related to the Saint-Venant torsion  $T_1$  by

$$T_1 = G I_T \theta'$$

where the torsional constant  $I_T$  (Saint-Venant torsional constant) is

$$I_T = \int_A \left[ (y - y_{sc})^2 + (z - z_{sc})^2 + (y - y_{sc}) \frac{\partial \omega}{\partial z} - (z - z_{sc}) \frac{\partial \omega}{\partial y} \right] dA$$

## 3 TOTAL DISPLACEMENT FIELD AND SHEAR STRAINS

### 3.1 Total axial displacement

At a point  $(x, y, z)$ :

$$u_{total}(x, y, z) = u_x(x) - y \varphi_z(x) + z \varphi_y(x) - \omega(y, z) \theta'(x) + u(x, y, z)$$

$$v(x, y, z) = v(x) - z \varphi_x(x) \quad w(x, y, z) = w(x) + (y - y_{sc}) \varphi_x(x)$$

$u_x(x)$  = axial displacement of the centroid

$\varphi_y(x), \varphi_z(x)$  = bending rotations (about  $y$  and  $z$ )

$\theta'(x)$  = rate of twist

$\omega(y, z)$  = primary warping function (from Section 1)

$u(x, y, z)$  = additional axial displacement (from Section 2)

### 3.2 Engineering shear strains (from total displacement)

Shear strains associated with shear stresses:

$$\gamma_{xy} = \frac{\partial u_{total}}{\partial y} + \frac{\partial v}{\partial x} = \left[ -(z - z_{sc}) - \frac{\partial \omega}{\partial y} \right] \theta' + \frac{\partial u}{\partial y}$$

$$\gamma_{xz} = \frac{\partial u_{total}}{\partial z} + \frac{\partial w}{\partial x} = \left[ (y - y_{sc}) - \frac{\partial \omega}{\partial z} \right] \theta' + \frac{\partial u}{\partial z}$$

## 5 REMARKS ON NONPRINCIPAL AXES

• Because  $I_{yz} \neq 0$ , the shear-force terms in Section 2 are coupled: the coefficients  $\alpha$  and  $\beta$  involve  $I_{yz}$ .

• The shear center  $(y_{sc}, z_{sc})$  is a property of the cross-section and is independent of the axis system.

• The warping function  $\omega$  is obtained by solving the Laplace equation with the Neumann condition in Section 1.

• Once  $\omega$  is known, the Poisson equation in Section 2 is solved for  $u$  with the natural boundary condition.

## 2 ADDITIONAL AXIAL DISPLACEMENT $u_x(x, y, z)$ DUE TO SHEAR FORCES $(V_y, V_z)$ AND WARPING TORSIONA MOMENT $T_w$

### 2.1 Weak (variational) formulation

Find  $u \in H^1(A)$  such that for all  $\delta u \in H^1(A)$ :

$$\int_A G \nabla \delta u \cdot \nabla u \, dA = \int_A \left[ \alpha y + \beta z + \frac{T_w}{J_w} \right] \delta u \, dA$$

where

$$\alpha = \frac{V_y I_z - V_z I_{yz}}{I_y I_z - I_{yz}^2}, \quad \beta = \frac{V_z I_y - V_y I_{yz}}{I_y I_z - I_{yz}^2}$$

$V_y, V_z$  = shear resultants in  $y$  and  $z$

$T_w$  = warping torsional moment

$I_y, I_z$  = second moments of area about  $y$  and  $z$

$I_{yz}$  = product of inertia (nonzero for nonprincipal axes)

$I_w$  = warping constant (sectorial moment of inertia)

$\omega(y, z)$  = primary warping function (from Section 1)

### 2.2 Strong formulation (Poisson equation)

The function  $u(x, y, z)$  satisfies:

$$-G \nabla^2 u = \alpha y + \beta z + \frac{T_w}{J_w} \quad \text{in } A$$

with natural boundary condition:

$$G \frac{\partial u}{\partial n} = 0 \quad \text{on } \partial A$$

**Important:**  $u$  depends on  $\alpha$  because  $\alpha, \beta$  (from  $V_y, V_z$ ) and  $\frac{T_w}{J_w}$  (from  $T_w$ ) depend on  $x$ .

Typically:  $V_y = V_y(x), V_z = V_z(x), T_w = T_w(x)$  so  $u = u(x, y, z)$ .

## 4 GENERAL EXPRESSIONS FOR SHEAR STRESSES

Using Hooke's law for shear:  $\tau = G \gamma$ .

### 4.1 Primary shear stresses (due to pure torsion $T_1$ )

$$\tau_{xy}^{prim} = G \left[ -(z - z_{sc}) - \frac{\partial \omega}{\partial y} \right] \theta', \quad \tau_{xz}^{prim} = G \left[ (y - y_{sc}) - \frac{\partial \omega}{\partial z} \right] \theta'$$

### 4.2 Secondary shear stresses (due to shear forces and warping torsion)

$$\tau_{xy}^{sec} = G \frac{\partial u}{\partial y}, \quad \tau_{xz}^{sec} = G \frac{\partial u}{\partial z}$$

### 4.3 Total shear stresses

$$\tau_{xy} = G \left[ -(z - z_{sc}) - \frac{\partial \omega}{\partial y} \right] \theta' + G \frac{\partial u}{\partial y}$$

$$\tau_{xz} = G \left[ (y - y_{sc}) - \frac{\partial \omega}{\partial z} \right] \theta' + G \frac{\partial u}{\partial z}$$

**Resultant shear stress at a point:**

$$\tau = \sqrt{\tau_{xy}^2 + \tau_{xz}^2}$$

## 6 SUMMARY OF THE SOLUTION PROCEDURE

- Solve for  $\omega(y, z)$ : Solve  $\nabla^2 \omega = 0$  in  $A$  with  $\frac{\partial \omega}{\partial n} = (y - y_{sc}) n_z - (z - z_{sc}) n_y$  on  $\partial A$ .
- Compute  $I_T$ : Evaluate  $I_T = \int_A \left[ (y - y_{sc})^2 + (z - z_{sc})^2 + (y - y_{sc}) \frac{\partial \omega}{\partial z} - (z - z_{sc}) \frac{\partial \omega}{\partial y} \right] dA$ .
- Solve for  $u(x, y, z)$ : Solve  $-G \nabla^2 u = \alpha y + \beta z + \frac{T_w}{J_w}$  in  $A$  with  $G \frac{\partial u}{\partial n} = 0$  on  $\partial A$ .
- Compute shear stresses: Use the total stress expressions in Section 4  $\tau_{xy}, \tau_{xz}$  (or keep in terms of  $\theta'$ ).
- Resultant shear stress:  $\tau = \sqrt{\tau_{xy}^2 + \tau_{xz}^2}$  at any point.

This framework is fully general for solid or thick-walled sections and provides the governing equations for shear, torsion, and warping in combined shear, torsion, and warping torsion.